

**FABE 5820 SECOND EXAM**  
**Open book, open notes**

Work rapidly. Present fundamental equations used. Show all work and units. Cite all assumptions and references. The point value of each question is shown in the margin (Total = 100 pts).

1. Design a mechanical ventilation system for a community theater house located in Bakersfield, California. Assume an exhaust ventilation system and 99% heating season design conditions. Given the following:

A/R<sub>t</sub> value for the building = 127 btu/hr °F  
 $t_i$  (design) = 70°F (winter) to 76°F (summer)  
RH<sub>i</sub> all-season design = 50%  
RH<sub>o</sub> winter design = 70%  
q<sub>s</sub> = 12,000 BTU/hr at all T<sub>i</sub> of interest  
q<sub>L</sub> = 5,056 BTU/hr at all T<sub>i</sub> of interest

100%  
PERFECT  
SCORE!

A. What winter ventilation rate would you specify (CFM)?  
(15 pts) Sketch your psych chart and show all work and logic. ✓

$$t_o = 35.0^\circ\text{F}$$

$$Q = \frac{13.5 \frac{A}{\text{hr}}}{\text{hr}} (5,056 \frac{\text{BTU}}{\text{hr}})$$

$$Q = 884.9 \frac{\text{cfm}}{\text{hr}}$$

Psych  
chart

Temp control

$$Q = \frac{V \cdot \dot{m}}{h_f g \cdot (1.0) (w_2 - w_1)}$$

From Psych chart @ indoor condition (1)  
(70°F and 50%)

$$w_2 = 0.0078 \frac{\text{lb}}{\text{lb dry}}$$

$$70.9 \cdot \text{RH}(1) \cdot$$

$$\cdot (1) 50\%, \text{RH}$$

$$w_2 = 0.0078$$

$$w_1 = 0.003$$

From Psych chart @ outdoor condition (2)  
(35°F and 70%)

$$w_1 = 21 \text{ grain} \frac{14.649}{46.49} \left( \frac{14.649}{100 \text{ grain}} \right) = 0.003 \frac{\text{lb}}{\text{lb dry}}$$

Exhaust ventilation by HRW, no mult w/ N. Windows

→ From Psych chart @ indoor condition  
(70°F and 50%)

$$V = 13.5 \frac{A}{\text{hr}}$$

From ASHRAE 2013,  $r = 1.9$ ,  $T_{DB} + 3$ ,  $\text{Q} = \dot{m} = 70^\circ\text{F}$ ,

$$h_f g = 1053.4 \frac{\text{BTU}}{\text{lb}}$$

round up to  
1054 BTU/lb

$$Q = 850 \text{ cfm}$$

Temp control

$$Q = \frac{V}{(100) (1.9) (70 - 35)} \left( \frac{1054}{12,000} \right) \frac{\text{cfm}}{\text{hr}}$$

$$Q = \frac{13.5 \frac{A}{\text{hr}}}{\text{hr}} (10.9 \cdot \frac{\text{BTU}}{\text{hr}}) (70 - 35)^\circ\text{F} / 12,000 \text{ BTU}$$

$$- (174 \frac{\text{BTU}}{\text{hr}}) (70 - 35)^\circ\text{F}$$

$$Q = 808.4 \text{ cfm} < 874.9 \text{ cfm}$$

$$Q = 874.9 \text{ cfm}$$

\* Use Table V at 14 pages! \*

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(5 pts) B. Assuming  $\Delta t = 10^\circ\text{F}$ , what fall-spring ventilation rate would you recommend for temperature control (CFM)?

$$Q = \frac{13.7 \frac{\text{BTU}}{\text{hr} \cdot \text{ft}^2}}{(100)(0.24 \frac{\text{BTU}}{\text{hr} \cdot \text{ft}^2})(10^\circ\text{F})} \left| \frac{12,000 \frac{\text{BTU}}{\text{hr}} - (13.7 \frac{\text{BTU}}{\text{hr} \cdot \text{ft}^2})(10^\circ\text{F})}{10^\circ\text{F}} \right| = \boxed{1005.1 \text{ CFM}}$$

round up to  $1050 \text{ CFM}$ ;  
 $\boxed{1050 \text{ CFM}}$

(5 pts) C. Assuming  $\Delta t = 5^\circ\text{F}$ , what summer ventilation rate would you recommend (CFM)?

$$Q = \frac{13.7 \frac{\text{BTU}}{\text{hr} \cdot \text{ft}^2}}{(100)(0.24 \frac{\text{BTU}}{\text{hr} \cdot \text{ft}^2})(5^\circ\text{F})} \left| \frac{12,000 \frac{\text{BTU}}{\text{hr}} - (13.7 \frac{\text{BTU}}{\text{hr} \cdot \text{ft}^2})(5^\circ\text{F})}{5^\circ\text{F}} \right| = \boxed{2130.9 \text{ CFM}}$$

round up to  $2150 \text{ CFM}$ ;  
 $\boxed{2150 \text{ CFM}}$

(15 pts) D. Assume that you can specify fans of any size and that you must use four fans. What fan sizes would you recommend and when would they turn on? Assume that the first three fans are for fall-spring conditions and colder and that all four fans will run for maximum summer conditions. None of the fans can provide variable output flow rates.

350 CFM to run continuously (for fall-spring condition) ( $= \frac{1050 \text{ CFM}}{3}$ )

350 CFM to turn on when  $t_i \geq 71^\circ\text{F} = 1050 \text{ CFM}$ )

350 CFM to turn on when  $t_i \geq 73^\circ\text{F} = 1050 \text{ CFM}$ )

✓ 1100 CFM to turn on when  $t_i \geq 75^\circ\text{F}$  ( $= 2150 \text{ CFM} - 1050 \text{ CFM}$ )

2. Calculate the temperature in an attic in Dublin, Ireland, at 99.6% winter design conditions where the temperature in the room below the attic is  $70^\circ\text{F}$ . Assume the attic is sealed tightly and has no natural or mechanical ventilation. The AU-values are as follows:

$$AU_{\text{roof}} = 113 \text{ BTU/hr}^\circ\text{F}$$

$$AU_{\text{gables}} = 345 \text{ BTU/hr}^\circ\text{F}$$

$$AU_{\text{ceiling}} = 733 \text{ BTU/hr}^\circ\text{F}$$

(10 pts)

No natural or mechanical ventilation

$$t_0 = 24.7^\circ\text{F}$$

$$q_{\text{ventilation}} = q_b - q_b$$

$$q_b = q_b$$

$$AU_{\text{roof}} \Delta t + AU_{\text{gables}} \Delta t = AU_{\text{ceiling}} \Delta t$$

$$(113 \frac{\text{BTU}}{\text{hr}^\circ\text{F}} + 345 \frac{\text{BTU}}{\text{hr}^\circ\text{F}})(t_i - 24.7^\circ\text{F}) = (733 \frac{\text{BTU}}{\text{hr}^\circ\text{F}})(70^\circ\text{F} - t_i)$$

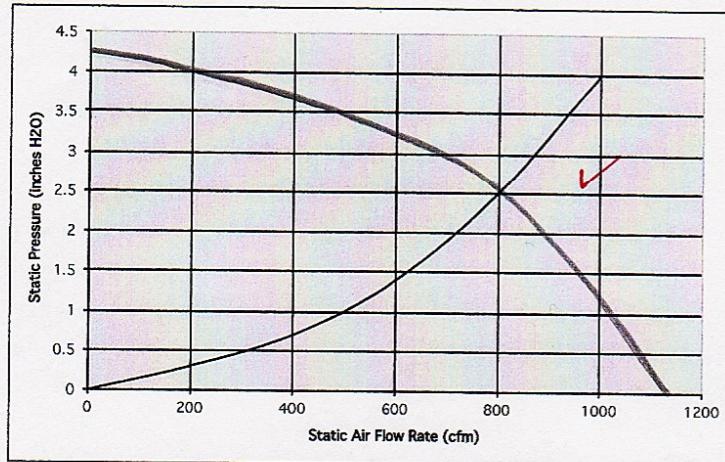
$$458t - 12457.4 = 51310 - 733t$$

$$\frac{1191t}{1191} = \frac{63757.4}{1191}$$

$$t_i = 53.5^\circ\text{F}$$

3. The characteristic curve for a duct system is presented below. Sketch in a hypothetical fan curve that would operate at the farmer's desired airflow rate of 800 CFM. Identify the operating point values (Q, P<sub>s</sub>) in the blanks below the graph.

(10 pts)



Operating Point = 800 CFM at 2.5 inches H<sub>2</sub>O static pressure

4. Using the appropriate fan laws (show your work and document all equations used), fill in the table below with four values showing how air flow rate and static pressure will change when an original fan is modified to increase fan diameter or speed.: (15 pts)

ORIGINAL FAN		Effect of changing diameter		Effect of changing speed	
D = 12 inches, N = 2000rpm	Q (cfm)	D = 20 inches, N = 2000rpm	Q (cfm)	D = 12 inches, N = 3000 rpm	Q (cfm)
400	0.5	1857 ✓	1.39 ✓	600 ✓	1.13 ✓

changing diameter, D

$$P_2 = P_1 \left( \frac{D_2}{D_1} \right)^2$$

$$Q_2 = Q_1 \left( \frac{D_2}{D_1} \right)^3$$

changing speed, N

$$P_2 = P_1 \left( \frac{N_2}{N_1} \right)^2$$

$$Q_2 = Q_1 \left( \frac{N_2}{N_1} \right)$$

$$P_2 = 0.5 \text{ in} \left( \frac{20 \text{ in}}{12 \text{ in}} \right)^2 = 1.39 \text{ in}$$

$$Q_2 = 400 \text{ cfm} \left( \frac{20 \text{ in}}{12 \text{ in}} \right)^3 = 1857 \text{ cfm}$$

$$= 600 \text{ cfm}$$

5. An Arabian horse stable outside of Dallas, Texas, has an internal sensible heat production of 33,740 BTU/hr, an AU-value of 715 BTU/hr°F, and a ventilation rate of 900 cfm. Indoor design temperature,  $T_i = 65^\circ\text{F}$ . Using the bin method, answer the following questions:

(5 pts) A. What is the balance point temperature,  $T_{o\text{(bal)}}$ ?

$$T_{o\text{(bal)}} = T_i - \sqrt{\frac{q_f}{AU + 1.08Q}} = 65^\circ\text{F} - \sqrt{\frac{33,740 \frac{\text{BTU}}{\text{hr}}}{715 \frac{\text{BTU}}{\text{hr°F}} + 1.08(900 \text{ cfm})}} = \boxed{45^\circ\text{F}}$$

(10 pts) B. How many actual hours would be used for the bin containing the balance point temperature?

1 hr bin  $\rightarrow$  night bin that includes  $T_i$  balanced temp.  $\rightarrow 45/49^\circ\text{F bin}$

$$h_{\text{act}} = h_{\text{bin}}(h_{\text{act}}) \left| \frac{t_{\text{bin}} - t_{\text{balance}}}{5^\circ\text{F}} \right) = 0.15h_{\text{act}} \left( \frac{45 - 44.5}{5^\circ\text{F}} \right) = 0.15h_{\text{act}}$$

$$\boxed{0.15 \text{ hour}}$$

✓

(10 pts) C. How much energy (MBTU, million BTUs) is required for the 32°F (30/34°F) bin?

$$30/34^\circ\text{F} - 32^\circ\text{F} = 2.8^\circ\text{F}$$

$$q_{\text{MBT}} = q_{\text{act}} + q_{\text{balance}} - q_f$$

$$\Delta t = T_i - T_{o\text{act}}$$

$$= 65 - 32 = 33^\circ\text{F}$$

$$= (33,740 \frac{\text{BTU}}{\text{hr}} + 23,571 \frac{\text{BTU}}{\text{hr}} - 33,740) \frac{\text{BTU}}{\text{hr}}$$

$$q_{\text{act}} = 1.08Q\Delta t$$

$$= 21,931 \frac{\text{BTU}}{\text{hr}}$$

$$= 1.08(900 \text{ cfm})(33^\circ\text{F})$$

$$E = q_{\text{MBT}} \times h_{\text{act}}$$

$$= 32,074 \frac{\text{BTU}}{\text{hr}}$$

$$= (21,931 \frac{\text{BTU}}{\text{hr}})(2.89 \text{ hour})$$

$$q_{\text{balance}} = AU\Delta t$$

$$= 43,780.5 \text{ BTU}$$

$$= (715 \frac{\text{BTU}}{\text{hr°F}})(33^\circ\text{F})$$

$$= \boxed{43.78 \text{ MBTU}}$$

$$= 23,595 \frac{\text{BTU}}{\text{hr}}$$